

SEPARATION PROCESS

DRYING Part 3

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Experimental Determination Rate Of Drying Curves

- solid placed on a tray
- only top surface exposed to air stream
- tray suspended from a balance
- record loss in weight during drying
- conditions closely resemble actual large-scale operations
 - ratio of drying to nondrying surface, bed depth, velocity, humidity, temperature, & direction of air.
- Free moisture content, X

$$\text{Moisture Content, } X_t = \frac{W - W_s}{W_s}$$

$$\text{Free Moisture Content, } X = X_t - X^*$$

Where W = weight of wet solid at given time, W_s = weight of dry solid

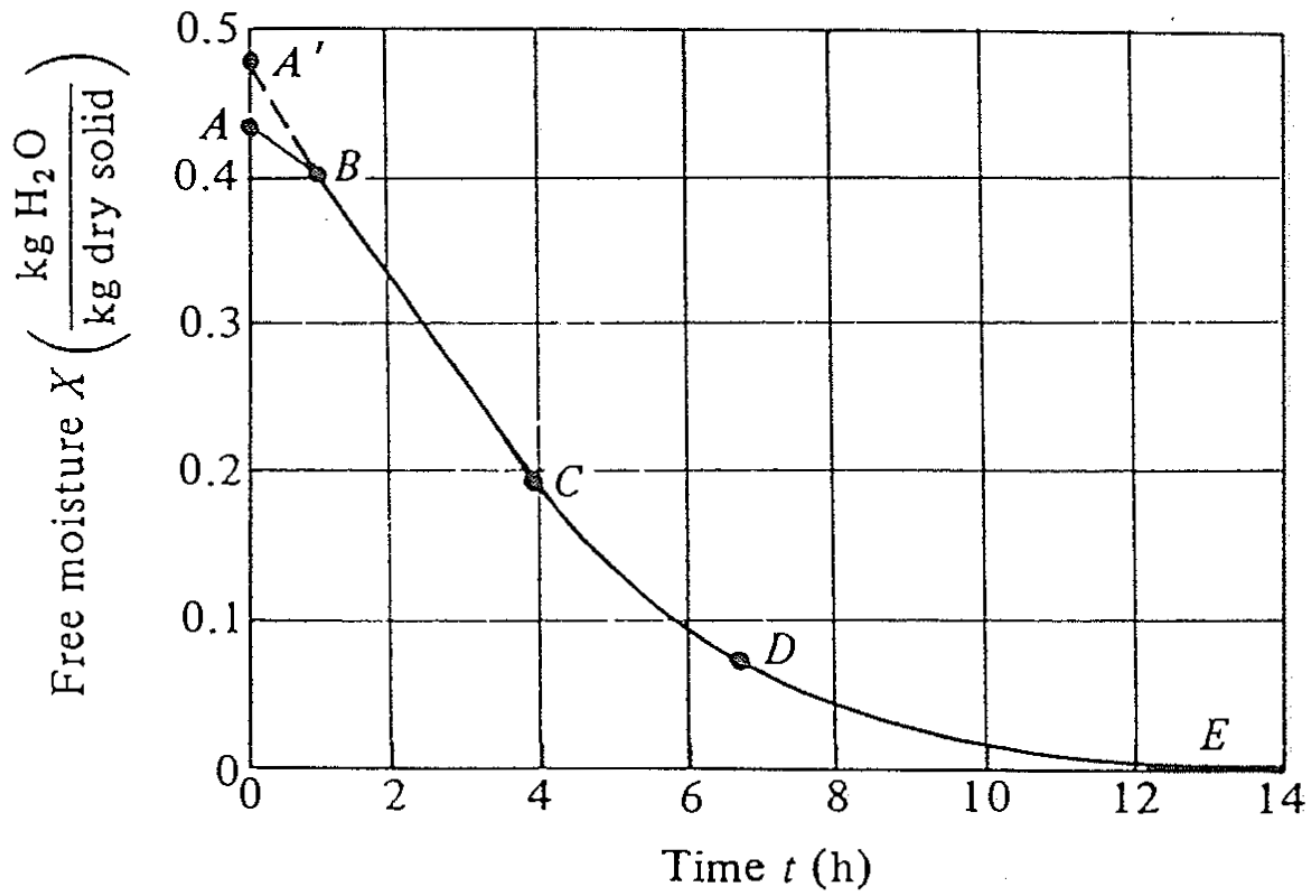
- To obtain rate of drying R : get slopes of tangents (dX/dt) at different values of t .

$$R = -\frac{L_s}{A} \frac{dX}{dt}$$

Where, L_s = kg of dry solid used; A = exposed surface area for drying.

Drying Rate Curve

Free Moisture Content vs Time

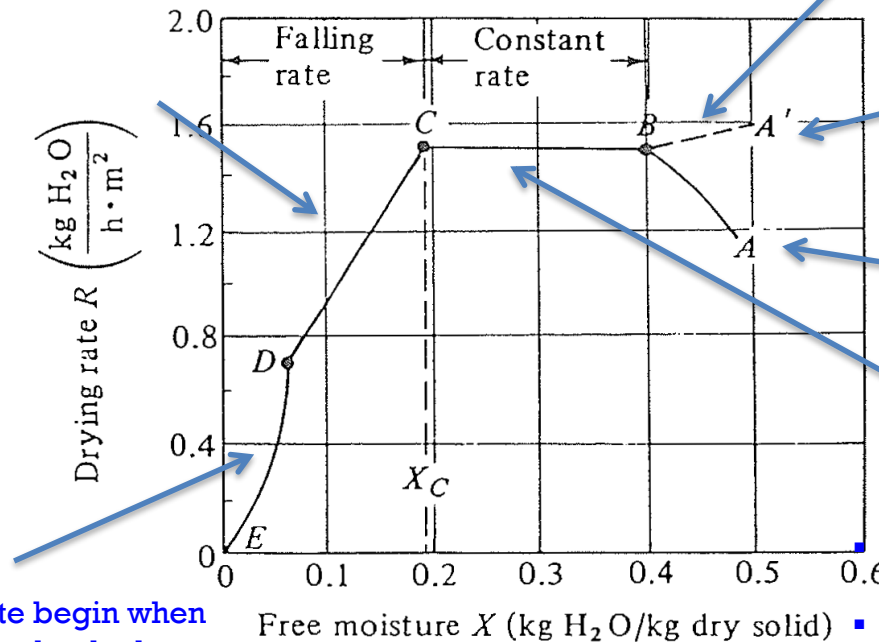


Drying Rate Curve

Rate vs Free Moisture Content

- X_c - critical free moisture content
- Insufficient water on surface for continuous film of water.
- Entire surface no longer wetted and the area continually decrease until the surface is completely dry
- Linear rate

Line A-B: unsteady-state adjustment period; short and often ignored



Point A' - initial free moisture content if solid if hot than the ultimate temp.

Point A - initial free moisture content if solid if cold than the ultimate temp.

- Second falling rate begin when the surface is completely dry
- Evaporation from interior of solid
- Sometimes, this rate is completely missing or may constitute with first falling rate period

Solid surface very wet initially and continuous film of water exist on drying surface.

- This water is entirely unbound water
- Rate of evaporation independent of the solid and same as rate of a free liquid surface.
- However, roughness of solid surface \square , rate \square .
- For porous surface, water continuously replaced by liquid from interior.

Calculation Methods For Constant-Rate Drying Period

Using Experimental Drying Curve

- For free moisture vs time plot
 - read off the time for specific initial and final moisture content
- Using rate of drying curve equation
 - Integrate over the time interval for drying from

$$X_{\text{initial}} \text{ to } X_{\text{final}} \quad R = -\frac{L_S}{A} \frac{dX}{dt}$$

rearrange

$$t = \int_{t_1}^{t_2} dt = \frac{L_S}{A} \int_{X_2}^{X_1} \frac{dX}{R}$$

$$t = \frac{L_S}{AR_C} (X_1 - X_2)$$

Calculation Methods For Constant-Rate Drying Period

Using Predicted Transfer Coefficients

- Drying occur by mass transfer of water vapor from saturated surface through an air film to the bulk gas phase
- The rate of moisture movement within the solid is sufficient to keep the surface saturated
- The rate of water vapor removal is controlled by the rate of heat transfer to the evaporating surface, which furnished the latent heat of vaporization
- At steady state, rate of mass transfer = rate of heat transfer.
- Assumptions:
 - Only **convective heat transfer to solid surface from hot gas to surface**.
 - Mass transfer is from surface to hot gas.

$$t = \frac{L_S \lambda_w (X_1 - X_2)}{Ah(T - T_w)} = \frac{L_S (X_1 - X_2)}{Ak_y M_B (H_w - H)}$$

$$R_C = \frac{q}{A \lambda_w} = \frac{h(T - T_w)}{\lambda_w} = k_y M_B (H_w - H)$$

A = exposed drying area (m^2)

T, T_w = temperature of gas & surface of solid, respectively ($^{\circ}C$).

λ_w = latent heat at T_w (J/kg)

M_A, M_B = molecular weight of water & air, respectively.

h = heat-transfer coefficient ($W/m^2.K$)

K_y = mass transfer coefficient ($kmol/s.m^2$)

H, H_w = humidity

Calculation Methods For Constant-Rate Drying Period

Using Predicted Transfer Coefficients

- It is found to be more reliable to use heat transfer coefficient, h than mass transfer coefficient since an error in determine the interface temperature T_w affects the driving force $(T-T_w)$ is less than it affects (H_w-H)

Case 1: Air flowing parallel to the drying surface

$$h = 0.0204G^{0.8} \text{ (SI)}$$

- Condition: $T = 45 - 150 \text{ }^\circ\text{C}$, $G = 2450 - 29,300 \text{ kg/h.m}^2$ (G , mass velocity = $v \rho$) $v = 0.61 - 7.6 \text{ m/s}$

Case 2: Air flowing perpendicular to the surface

$$h = 1.17G^{0.37} \text{ (SI)}$$

- Condition: $G = 3900 - 19,500 \text{ kg/h.m}^2$; $v = 0.9 - 4.6 \text{ m/s}$

Combined Convection, Radiation and Conduction Heat Transfer in Constant Rate Period

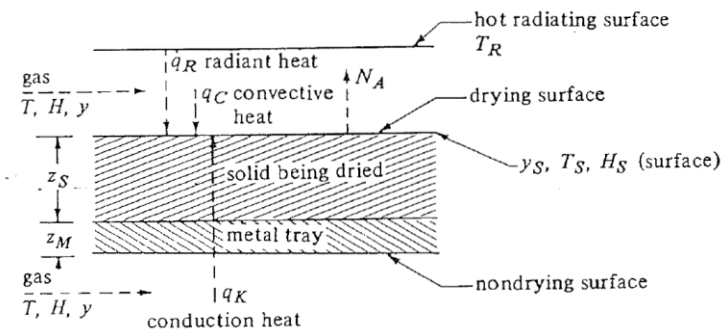
- Total rate of heat transfer to the drying surface is

$$q = q_c + q_R + q_K$$

q_c – convective heat transfer from gas T to the solid surface T_s

q_R – radiant heat transfer from the surface at T_R to T_s

q_K – conduction heat transfer from the bottom



$$q_c = h_c(T - T_s)A$$

$$q_R = h_R(T_R - T_s)A$$

$$h_R = e(5.676) \frac{\frac{\sigma T(K)_R}{100}^4 - \frac{\sigma T(K)_S}{100}^4}{T_R - T_s}$$

$$R_C = \frac{q}{A/S} = \frac{(h_c + U_K)(T - T_s) + h_R(T_R - T_s)}{I_S} = k_y M_B (H_S - H)$$

$$\frac{(H_S - H)I_S}{h_c / k_y M_B} = (1 + U_K / h_c)(T - T_s) + (h_R / h_c)(T_R - T_s)$$

$$h_c / k_y M_B = cS = (1.005 + 1.88H)103$$

$$q_K = U_K(T - T_s)A$$

$$U_K = \frac{1}{1/h_c + z_M/k_M + z_S/k_S}$$

z_M – metal thickness in m, k_M – metal thermal conductivity in W/m.K, z_S – solid thickness in m, k_S – solid thermal conductivity, h_c assumed to be same as convective heat transfer coefficient

Credit to the authors:
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