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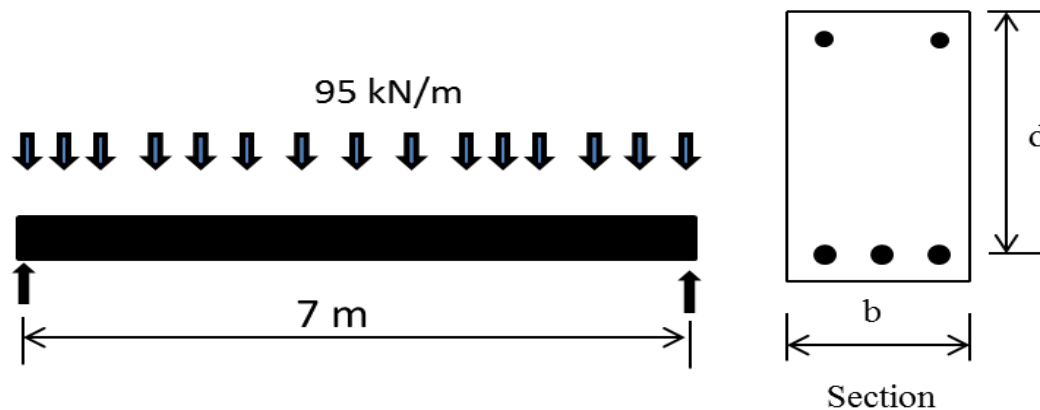
# REINFORCED CONCRETE DESIGN 1

## Shear Design (Examples and Tutorials) by

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# Example 1: Section requiring shear reinforcement design

A simply supported beam of 7 m span carries a uniform ultimate load of 95 kN/m. The beam dimensions are 200 x 450 mm ( $b \times d$ ) and the longitudinal reinforcement provided are 3H20 and 2H12 for tension and compression respectively. Design the shear reinforcement using vertical links. Use  $f_{ck} = 25 \text{ N/mm}^2$  and  $f_{yk} = 500 \text{ N/mm}^2$ .



# Example 1: Section requiring shear reinforcement design

Design shear force,  
 $V_{ED} = wL / 2 = 95 \times 7 / 2 = 332.5 \text{ kN}$

Concrete strut capacity

$$V_{Rd, \max} = \frac{0.36b_w d f_{ck} (1 - f_{ck}/250)}{(\cot \theta + \tan \theta)}$$

$$= 251 \text{ kN} \quad \text{-----} \quad \theta = 22 \text{ deg} \quad \cot \theta = 2.5$$

$$= 364 \text{ kN} \quad \text{-----} \quad \theta = 45 \text{ deg} \quad \cot \theta = 1.0$$

$$V_{Ed} > V_{Rd, \max} \cot \theta = 2.5$$

$$V_{Ed} < V_{Rd, \max} \cot \theta = 1.0$$

Therefore angle  $\theta > 22^\circ$

# Example 1: Section requiring shear reinforcement design

$$\begin{aligned}\theta &= 0.5 \sin^{-1} [V_{Ed} / 0.18 b_w d f_{ck} (1 - f_{ck} / 250)] \\ &= 0.5 \sin^{-1} [332.5 \times 103 / 0.18 \times 200 \times 450 \times 25 \\ &\quad \times (1 - 25 / 250)] \\ &= 33^\circ\end{aligned}$$

$$\text{Use : } \theta = 33^\circ \quad \tan \theta = 0.65 \quad , \quad \cot \theta = 1.54$$

## Shear links

$$\begin{aligned}A_{sw} / s &= V_{Ed} / 0.78 f_{yk} d \cot \theta \\ &= 332.5 \times 103 / (0.78 \times 500 \times 450 \times 1.54) \\ &= 1.23\end{aligned}$$

# Example 1: Section requiring shear reinforcement design

Try links: H8,  $A_{sw} = 101 \text{ mm}^2$   
Spacing,  $s = A_{sw}/1.23 < 0.75d$   
 $= 82 \text{ mm} < 0.75 (450)$   
 $= 337.5 \text{ mm}$

Max. spacing, Use  $s_{max} = 75 \text{ mm}$

Provide: H8-75

## Minimum links

$$\begin{aligned} A_{sw} / s &= 0.08 f_{ck}^{1/2} b_w / f_{yk} \\ &= (0.08 \times 25^{1/2} \times 200) / 500 \\ &= 0.16 \end{aligned}$$

# Example 1: Section requiring shear reinforcement design

Try links : H8,  $A_{sw} = 101 \text{ mm}^2$

$$\begin{aligned}\text{Spacing, } s &= 101/0.16 \\ &= 631 \text{ mm} < 0.75d \\ &= 337 \text{ mm}\end{aligned}$$

Provide: H8-325

Shear resistance of minimum links

$$\begin{aligned}V_{\min} &= (A_{sw}/s) (0.78df_{yk} \cot \theta) \\ &= (101/325) (0.78 \times 400 \times 500 \times 2.5) \\ &= 121 \text{ kN}\end{aligned}$$

# Example 1: Section requiring shear reinforcement design

Additional longitudinal reinforcement

Additional tensile force,

$$\begin{aligned}F_{td} &= 0.5 V_{Ed} \cot \theta \\ &= 0.5 \times 332.5 \times 1.54 \\ &= 256 \text{ kN}\end{aligned}$$

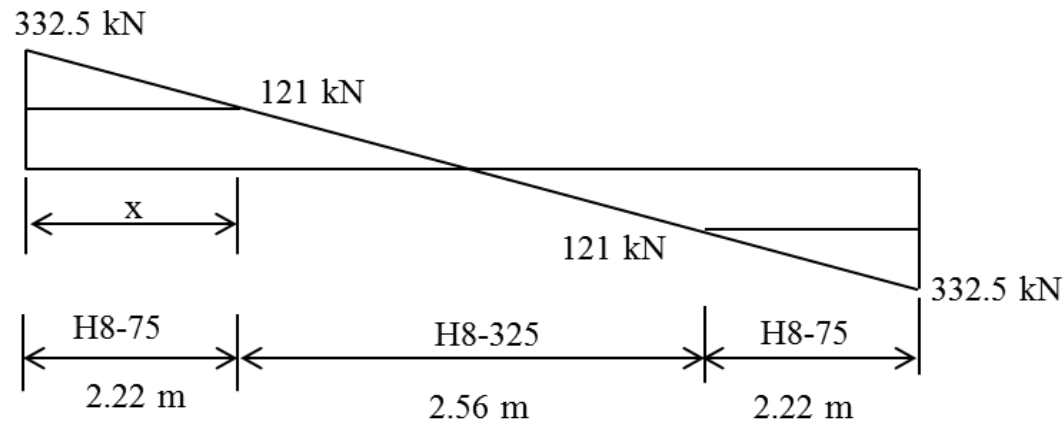
Additional tension reinforcement,

$$\begin{aligned}A_s &= F_{td} / 0.87 f_{yk} \\ &= 256 \times 10^3 / (0.87 \times 500) \\ &= 588 \text{ mm}^2\end{aligned}$$

Use: 2H20 ( $A_s = 626 \text{ mm}^2$ )

To be added to  $A_s$  for flexure support (after curtailment)

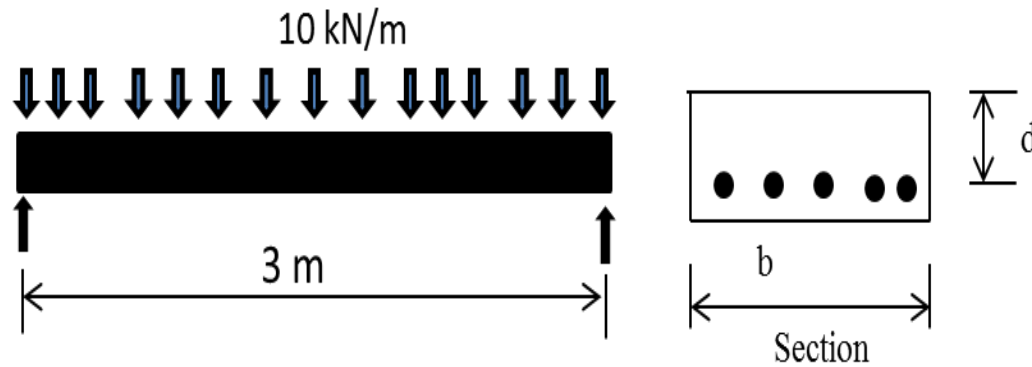
# Example 1: Section requiring shear reinforcement design



$$x = (332.5 - 121) / 95 = 2.22 \text{ m}$$



# Example 2: Section not requiring shear reinforcement design



A 3 m span simply supported slab with effective depth  $d = 125$  mm carries an ultimate action of 10 kN/m per m width. The provided tension reinforcement steel is H8-150 bar. Use  $f_{ck} = 25$  N/mm<sup>2</sup> and  $f_{yk} = 500$  N/mm<sup>2</sup>. Verify shear reinforcement for this section.

## Example 2: Section not requiring shear reinforcement design

Span,  $L$  = 3.0 m

Size,  $b \times d$  = 1000 x 125 mm

Design load,  $w$  = 10 kN/m per m width

Characteristic strength of concrete,  $f_{ck}$  = 25 N/mm<sup>2</sup>

Characteristic strength of steel,  $f_{yk}$  = 500 N/mm<sup>2</sup>

Tension steel : **H8 – 150** ,  $A_s$  = 335 mm<sup>2</sup>

## Example 2: Section not requiring shear reinforcement design

Design shear force,  $V_{Ed}$

$$V_{Ed} = wL/2 = 10 \times 3 / 2 = 15 \text{ kN}$$

Concrete shear resistance

$$\begin{aligned} V_{Rdc} &= [0.12 k (100 \rho_1 f_{ck})^{1/3}] b_w d \\ &= 1 + (200/d)^{1/2} \leq 2.0 \\ &= 2.26 \leq 2.0 \end{aligned}$$

$$\begin{aligned} \rho_1 &= (A_{sl} / b_w d) \leq 0.02 \\ &= 0.0027 \leq 0.02 \end{aligned}$$

## Example 2: Section not requiring shear reinforcement design

$$\begin{aligned} V_{Rdc} &= [0.12 \times 2.0 \times (100 \times 0.0027 \times 25)^{1/3}] 1000 \times 125 \\ &= 56.7 \text{ kN} \end{aligned}$$

$$\begin{aligned} V_{min} &= [0.035 k^{3/2} f_{ck}^{1/2}] b_w d \\ &= [0.035 \times 2.0^{3/2} \times 25^{1/2}] 1000 \times 125 \\ &= 61.87 \text{ kN} \end{aligned}$$

$$\text{So, } V_{Rdc} = 61.87 > V_{ed} = 15$$

Therefore, shear check pass. No shear reinforcement is required!

# Tutorial

A rectangular reinforced concrete beam for a simply supported beam has a size of 150 mm width and 225 mm effective depth. If the beam is 3.3 m carrying a uniform distributed load of 10 kN/m<sup>2</sup>, calculate the area of steel required for shear reinforcement of this beam. Consider  $f_{ck} = 25 \text{ N/mm}^2$  and  $f_{yk} = 500 \text{ N/mm}^2$ .

# Examples and Tutorial