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REINFORCED CONCRETE DESIGN 1

Design of Beam (Examples and Tutorials) by

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Example 1: Simply supported beam design - Rectangular

A rectangular reinforced concrete beam simply supported on two masonry walls 200 mm thick and 6 m apart. The beam has to carry a distributed permanent action of 10 kN/m (excluding beam self-weight) and variable action of 8 kN/m. The beam is inside building subject to a 1 hour fire resistance and design for 50 years design life. Design the beam with deflection and crack check. Illustrate the beam detailing. Use concrete characteristic strength, $f_{ck} = 30 \text{ N/mm}^2$ and steel characteristic strength, $f_{yk} = 500 \text{ N/mm}^2$

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Specification

Effective span, $L = 6 \text{ m}$

Characteristic action:

Permanent, $g_k = 15 \text{ kN/m}$

Variable, $q_k = 10 \text{ kN/m}$

Design Life = 50 years

Fire resistance = R60

Exposure classes = XC1

Materials

Concrete Char. strength, $f_{ck} = 30 \text{ N/mm}^2$

Steel char. strength, $f_{yk} = 500 \text{ N/mm}^2$

Links char. strength, $f_{yk} = 500 \text{ N/mm}^2$

Reinforced concrete unit weight = 25
 kN/m^3

Use , $\phi_{\text{bar } 1} = 20 \text{ mm}$

$\phi_{\text{bar } 2} = 12 \text{ mm}$

$\phi_{\text{links}} = 8 \text{ mm}$

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Beam Size

Overall depth, $h = L/14 = 6000/13 = 462$ mm

Width, $b = 0.4 (h) = 0.4 \times 462 = 185$ mm

Try: $b \times h = 200 \times 500$ mm

Durability, Fire & Bond Requirements

Min. cover with regards to bond, $C_{\min,b} = 20$ mm

Min. cover with regards to durability, $C_{\min,dur} = 15$ mm

Min. required axis distance for R60 fire resistance, a_{sd}

$$a_{sd} = 30 + 10 = 40 \text{ mm}$$

Min. cover regards to fire, $C_{\min} = a_{sd} - \phi_{links} - \phi_{bar}/2$
 $= 40 - 8 - 20/2 = 22$ mm

Allowance in design for deviation, $\Delta C_{dev} = 10$ mm

Nominal cover, C_{nom}

$$C_{nom} = C_{\min} + \Delta C_{dev} = 22 + 10 = 32 \text{ mm}$$

Use: $C_{nom} = 35$ mm

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LOADING & ANALYSIS

$$\text{Beam self-weight} = 0.2 \times 0.5 \times 25 = 2.5 \text{ kN/m}$$

$$\text{Permanent load (Excluding self-weight)} = 10 \text{ kN/m}$$

$$\text{Total Charc. Permenant action} = \underline{12.5 \text{ kN/m}}$$

$$\text{Charc. Variable action} = 8 \text{ kN/m}$$

$$\text{Design Action, } w_d = 1.35 g_k + 1.5q_k = \mathbf{28.88 \text{ kN/m}}$$

Shear force, V

$$V = w_d L / 2 = 28.88 * 6 / 2 = 86.64 \text{ kN}$$

Bending Moment, M

$$M = W_d L^2 / 8 = 28.88 \times 6^2 / 8 = 130 \text{ kNm}$$

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MAIN REINFORMENT

Effective depth,

$$d = h - C_{\text{nom}} - \phi_{\text{link}} - \phi_{\text{bar}}/2 = 500 - 35 - 8 - 20/2 = 447 \text{ mm}$$

$$d' = C_{\text{nom}} + \phi_{\text{link}} + \phi_{\text{bar}}/2 = 35 + 8 + 20/2 = 53 \text{ mm}$$

Design bending moment, $M_{\text{Ed}} = 193 \text{ kNm}$

$$K = M / bd^2 f_{\text{ck}}, \quad K_{\text{bal}} = 0.167$$

$$= 130 \times 10^6 / (200 \times 447^2 \times 30)$$

$$= 0.108 < K_{\text{bal}} : \text{No compression reinforcement required}$$

$$z = d [0.5 + (0.25 - K/1.134)^{1/2}]$$

$$= 0.89 d = 0.89 \times 447$$

$$= 398 \text{ mm}$$

$$x = (d - z) / 0.4 = 191 \text{ mm}$$

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Area of tension steel

$$\begin{aligned} A_s &= M / 0.87 f_{yk} z \\ &= 130 \times 10^6 / (0.87 \times 500 \times 398) \\ &= 751 \text{ mm}^2 \end{aligned}$$

Use :

3H20 ($A_s = 943 \text{ mm}^2$)

Minimum and maximum reinforcement area,

$$\begin{aligned} A_{s_{\min}} &= 0.26 (f_{ctm} / f_{yk}) b d \\ &= 0.26 (2.9 / 500) b d > 0.0013 b d \\ &= 0.0015 b d > 0.0013 b d \text{ use } 0.0015 b d \\ &= 135 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} A_{s_{\max}} &= 0.04 A_c = 0.04 \times b \times h = 0.04 \times 200 \times 500 \\ &= 4000 \text{ mm}^2 \end{aligned}$$

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SHEAR REINFORCEMENT

Design shear force, $V_{Ed} = 86.64$ kN

Concrete strut capacity

$$V_{Rd, max} = \frac{0.36b_w f_{ck} (1 - f_{ck}/250)}{(\cot \theta + \tan \theta)}$$

$$= 655 \text{ kN} \quad \text{-----} \quad \theta = 22 \text{ deg} \quad \cot \theta = 2.5$$

$$= 950 \text{ kN} \quad \text{-----} \quad \theta = 45 \text{ deg} \quad \cot \theta = 1.0$$

$$V_{Ed} < V_{Rd, max} \quad \cot \theta = 2.5$$

$$V_{Ed} < V_{Rd, max} \quad \cot \theta = 1.0$$

--- Therefore angle $\theta = 22^\circ$

Example 1: Simply supported beam design - Rectangular

Shear links

$$\begin{aligned}A_{sw} / s &= V_{Ed} / 0.78 f_{yk} d \cot \theta = 0.513 V_{Ed} / f_{yk} d \\ &= 0.513 \times 86.64 \times 10^3 / (500 \times 447) \\ &= 0.199\end{aligned}$$

Use links: H8. $A_{sw} = 101 \text{ mm}^2$

$$\begin{aligned}\text{Spacing, } s &= A_{sw} / 0.199 = 101 / 0.199 \\ &= 508 \text{ mm}\end{aligned}$$

Maximum spacing, $S_{vmax} = 0.75d = 335 \text{ mm} < 508 \text{ mm}$: use 300 mm

Use: H8 - 300

Example 1: Simply supported beam design - Rectangular

Additional longitudinal reinforcement

Additional tensile force,

$$\begin{aligned} F_{td} &= 0.5 V_{Ed} \cot \theta = 0.5 \times 86.64 \times 10^3 \times 2.5 \\ &= 108.3 \text{ kN} \end{aligned}$$

Additional tension reinforcement,

$$\begin{aligned} A_s &= F_{td} / 0.87 f_{yk} = 108.3 \times 10^3 / (0.87 \times 500) \\ &= 249 \text{ mm}^2 \end{aligned}$$

Use :1H20 ($A_s = 314 \text{ mm}^2$)

To be added to the A_s near support (after curtailment)

Example 1: Simply supported beam design - Rectangular

DEFLECTION

Percentage of required tension reinforcement

$$\rho = A_{s \text{ req}} / bd = 751 / (200 \times 447) = 0.0084$$

Reference reinforcement ratio.

$$\rho_o = (f_{ck})^{1/2} \times 10^{-3} = (30)^{1/2} \times 10^{-3} = 0.0055$$

Factor for structural system , $K = 1.0$

$$\rho_o = 0.0055 < \rho = 0.0084$$

$$\text{Use } \frac{l}{d} = K \left[11 + 1.5 \sqrt{f_{ck}} \frac{\rho_o}{\rho - \rho'} + \frac{1}{12} \sqrt{f_{ck}} \sqrt{\frac{\rho'}{\rho}} \right]$$

$$\begin{aligned} l/d &= 1.0 [11 + (1.5 (30)^{1/2} \times 0.655) + 3.2 \times (30)^{1/2} \times (0)^{1/2}] \\ &= 1.0 [11 + 5.38 + 0] = 16.38 \end{aligned}$$

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Therefore basic span-effective depth ratio , $l/d = 16.38$

Modification factor for steel area provided,

$$\text{- Tension} = A_{s_{\text{prov}}} / A_{s_{\text{req}}} = 943 / 751 = 1.26 < 1.5$$

Therefore allowable span effective depth, $(l/d)_{\text{allowable}}$

$$(l/d)_{\text{allowable}} = 16.38 \times 1.26 = 20.64$$

Actual span effective depth, $(l/d)_{\text{actual}}$

$$(l/d)_{\text{actual}} = 6000/447 = 13.42$$

$$(l/d)_{\text{allowable}} > (l/d)_{\text{actual}} \rightarrow \text{OK}$$

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CRACKING

Limiting crack width, $w_{\max} = 0.3 \text{ mm}$

Steel stress, f_s

$$\begin{aligned} f_s &= \frac{f_{yk}}{1.15} \times \frac{Gk + 0.3Qk}{(1.35Gk + 1.5Qk)} \frac{1}{\delta} = \frac{500}{1.15} \times \frac{12.5 + 0.3 \times 8}{(1.35(12.5) + 1.5(8))} \\ &= 224 \text{ N/mm}^2 \end{aligned}$$

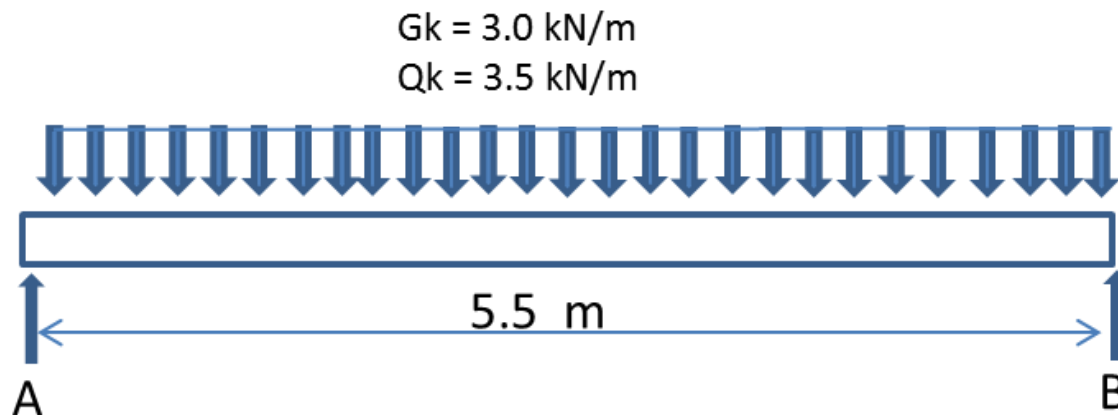
Max. allowable bar spacing = 200 mm

$$\begin{aligned} \text{Actual bar spacing, } s &= [h - 2(C_{\text{nom}}) - 2(\phi_{\text{links}}) - 20]/2 \\ &= [200 - 2(35) - 2(8) - 20]/2 = 47 \text{ mm} \end{aligned}$$

Actual = 47 mm < Allow, 200 mm → OK

Tutorial 1: Simply supported beam

Figure below shows a 5.5 m simply supported beam with size of 150 x 350 mm. The characteristic permanent and variable action acting on the beam are 3.0 kN/m (excluding self-weight and brick wall) and 3.5 kN/m. This beam has to support the brick wall with 3.3 m height.



Tutorial 1: Simply supported beam

The properties of the beam are as follows:

$$\text{Unit weight of concrete} = 25 \text{ kN/m}^3$$

$$\text{Unit weight of brick wall} = 2.6 \text{ kN/m}^2$$

$$\text{Concrete characteristic strength, } f_{ck} = 25 \text{ N/mm}^2$$

$$\text{Steel characteristic strength, } f_{yk} = 500 \text{ N/mm}^2$$

$$\text{Nominal cover, } c_{nom} = 25 \text{ mm}$$

$$\text{Use main reinforcement, } \phi_{main} = 20 \text{ mm}$$

$$\text{Use shear reinforcement, } \phi_{link} = 6 \text{ mm}$$

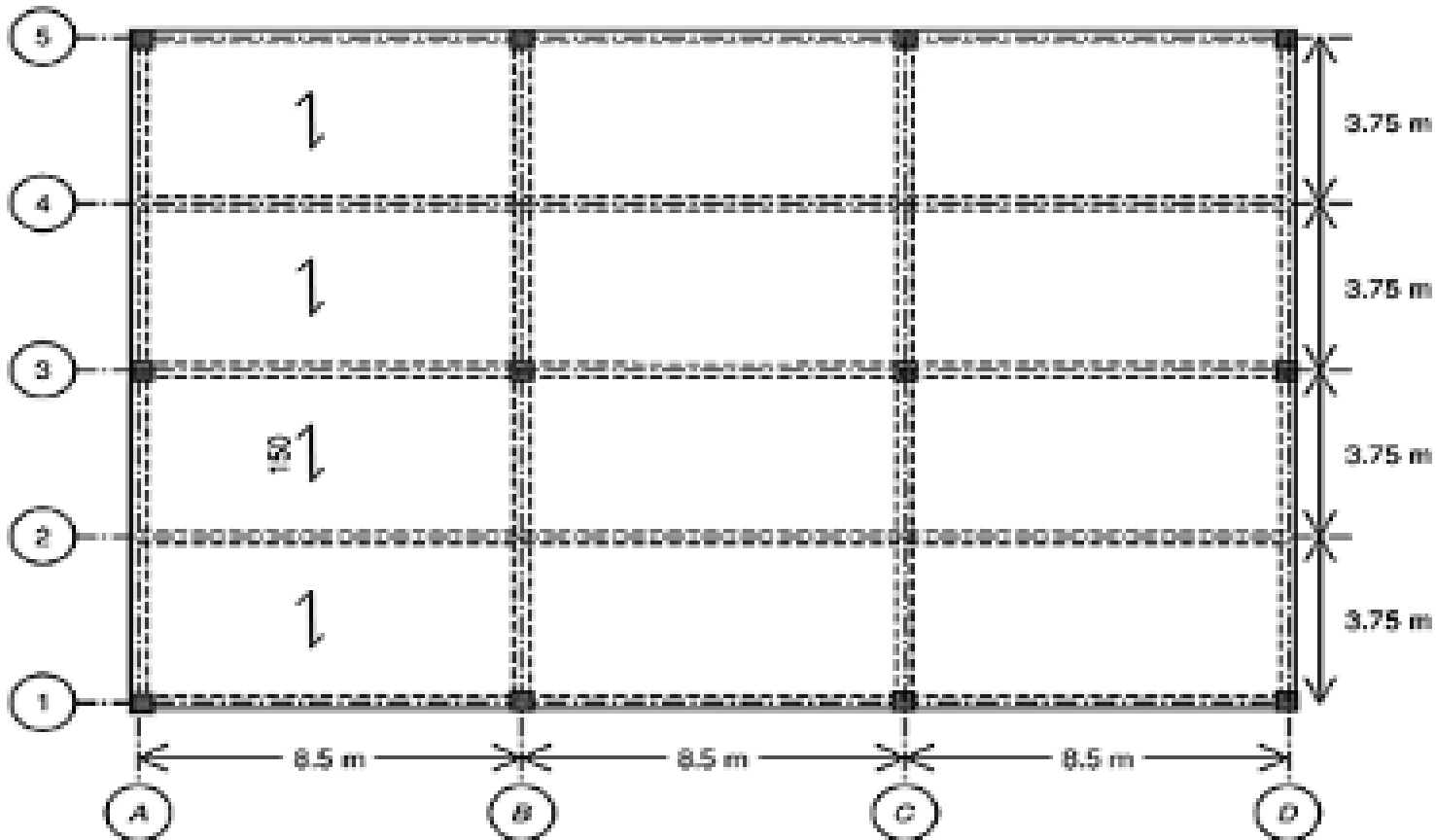
Tutorial 1: Simply supported beam

By using the data above,

- a) Calculate design load, bending moment and shear force for the beam
- b) Provide the main reinforcement for the beam
- c) Provide the shear reinforcement for the beam
- d) Check the beam due to the deflection
- e) Sketch the detailing for this beam

Tutorial 2: Continuous beam

Design the continuous beam (3/A-D) in figure below with beam detailing.



Tutorial 2: Continuous beam

The beam and slab will be casted monolithically. Use the following data to design the beam.

$$f_{ck} = 30 \text{ N/mm}^2$$

$$f_{yk} = 500 \text{ N/mm}^2$$

$$\text{Cover, } c = 25 \text{ mm}$$

$$\phi_{\text{main reinforcement}} = 8 \text{ mm}$$

$$q_{k,\text{slab}} = 1.5 \text{ kN/m}^2$$

$$\text{Slab finishing} = 1.0 \text{ kN/m}^2$$

$$\text{Slab thickness, } h_{\text{slab}} = 150 \text{ mm}$$

$$\text{beam size, } b \times h = 150 \times 400 \text{ mm}$$

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