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THEORY OF STRUCTURES

CHAPTER 2 : DEFLECTION (UNIT LOAD METHOD)

PART 2

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Chapter 2 : Part 2 – Unit Load Method

- Aims
 - Determine the slope and deflection by using Unit Load Method
- Expected Outcomes :
 - Able to analyze determinate beam – deflection and slope by Unit Load Method
- References
 - Mechanics of Materials, R.C. Hibbeler, 7th Edition, Prentice Hall
 - Structural Analysis, Hibbeler, 7th Edition, Prentice Hall
 - Structural Analysis, SI Edition by Aslam Kassimali,Cengage Learning
 - Structural Analysis, Coates, Coatie and Kong
 - Structural Analysis - A Classical and Matrix Approach, Jack C. McCormac and James K. Nelson, Jr., 4th Edition, John Wiley



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Principle of Virtual Work

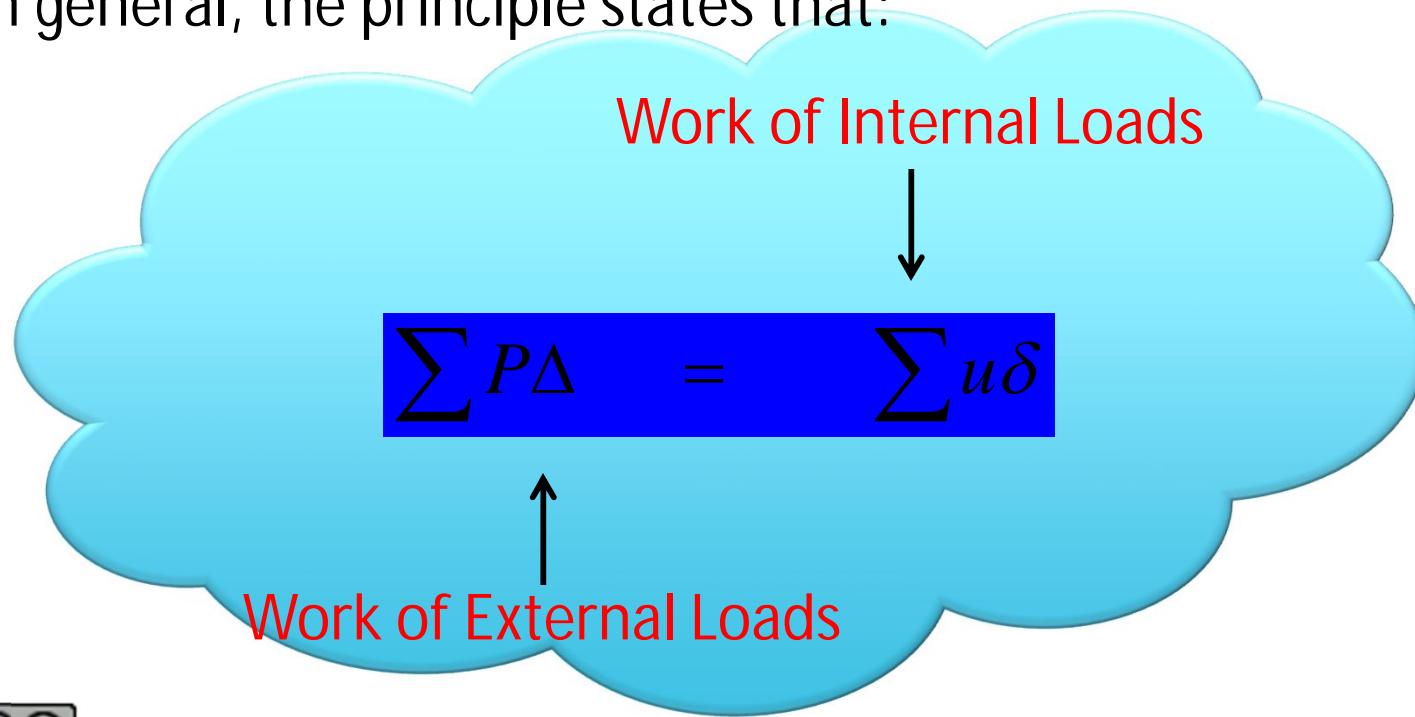
- The internal work in transversely loaded beams is taken equal to the strain energy due to bending moment
- The virtual force F_i in the i^{th} mass element in $\Delta = F^* e_i$ may be taken equal to the bending moment m_{ij} in the i^{th} mass element due to a unit load at coordinate j



Principle of Virtual Work

(Displacement)

- Sometimes referred as the Unit-Load Method
- Generally provides of obtaining the displacement and slope at a specific point on structure i.e. beam, frame or truss
- In general, the principle states that:


$$\sum P\Delta = \sum u\delta$$



Principle of Virtual Work (Displacement)

- Consider the structure (or body) to be of arbitrary shape
- Suppose it is necessary to determine the displacement Δ of point A on the body caused by the “real loads” P_1 , P_2 and P_3



Principle of Virtual Work

(Displacement)

- Since no external load acts on the body at A and in the direction of the displacement Δ , the displacement can be determined by first placing on the body a “virtual” load such that this force P' acts in the same direction as Δ , (see Figure)



Principle of Virtual Work

(Displacement)

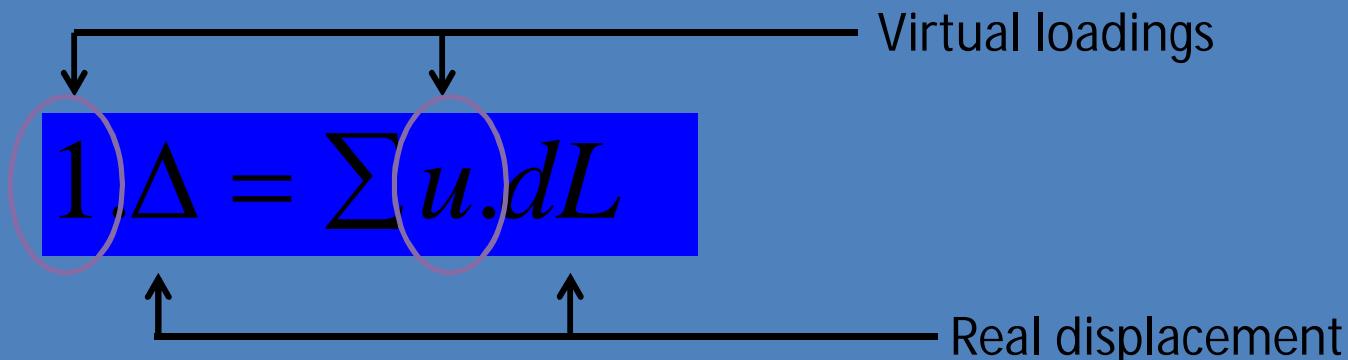
- We will choose P' to have a unit magnitude, $P' = 1$
- Once the virtual loadings are applied, then the body is subjected to the real loads P_1 , P_2 and P_3 , (see Figure)
- Point A will be displaced an amount Δ causing the element to deform an amount dL



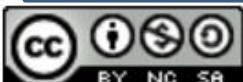
Principle of Virtual Work

(Displacement)

- As a result, the external virtual force P' & internal load u "ride along" by Δ and dL and therefore, perform external virtual work of $1 \cdot \Delta$ on the body and internal virtual work of $u \cdot dL$ on the element


$$1 \cdot \Delta = \sum u \cdot dL$$

- By choosing $P' = 1$, it can be seen from the solution for Δ follows directly since $\Delta = \sum u dL$



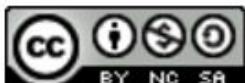
Principle of Virtual Work (Slope)

- A virtual couple moment M' having a unit magnitude is applied at this point
- This couple moment causes a virtual load u_θ in one of the elements of the body



Principle of Virtual Work (Slope)

- Assuming that the real loads deform the element an amount dL , the rotation θ can be found from the virtual-work equation

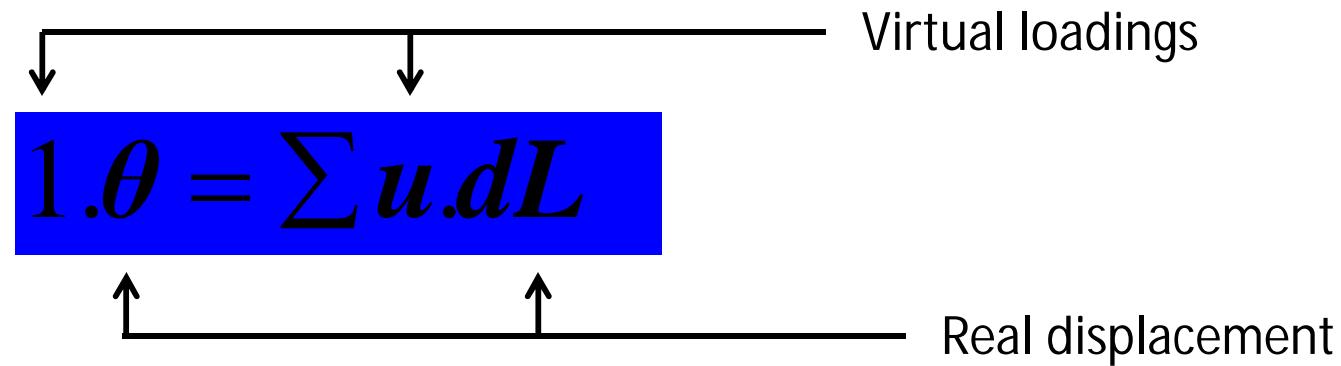


Principle of Virtual Work (Slope)

$$1.\theta = \sum u.dL$$

Virtual loadings

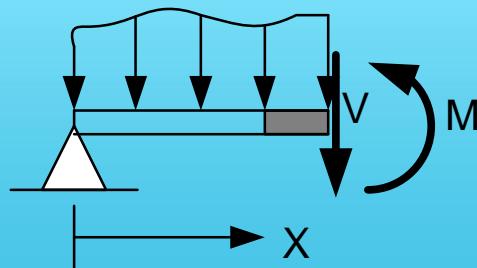
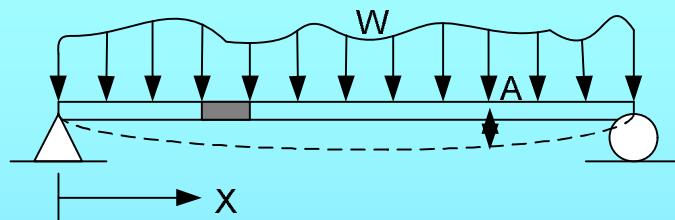
Real displacement



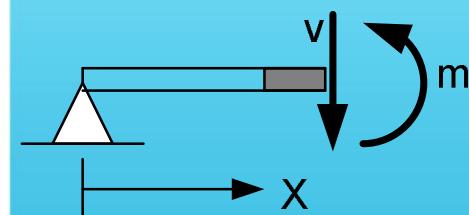
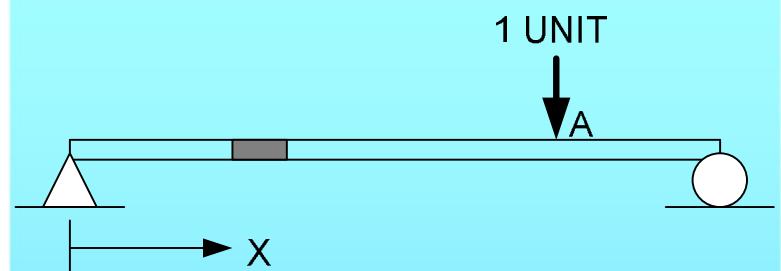


PRINCIPLE OF UNIT LOAD METHOD

REAL LOAD



VIRTUAL LOAD



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- The element deform or rotate $d\theta = (M / EI) dx$
- The external virtual work done by the unit load is $1 \cdot \Delta$
- The internal virtual work done by the moment, m

$$m d\theta = m(M/EI) dx$$

$$1 \cdot \Delta = \int_0^L \frac{mM}{EI} dx$$

Similarly

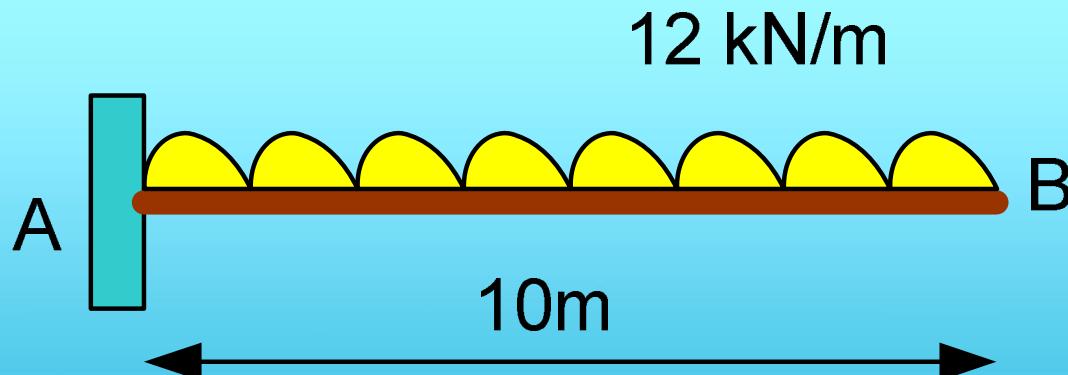
$$1 \cdot \theta = \int_0^L \frac{mM}{EI} dx$$



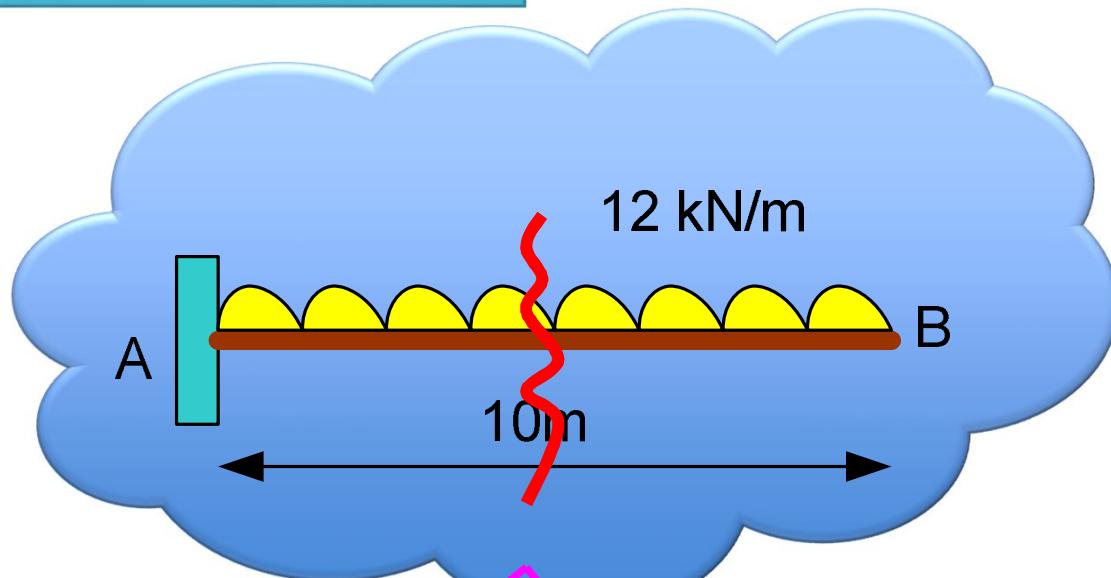
Example 1

Determine the displacement at point B of the steel beam shown in figure.

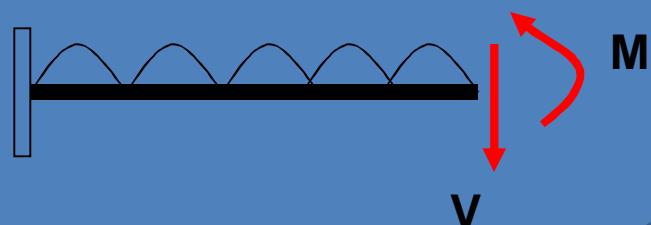
Take $E = 200\text{GPa}$, $I = 500 \times 10^6 \text{ mm}^4$



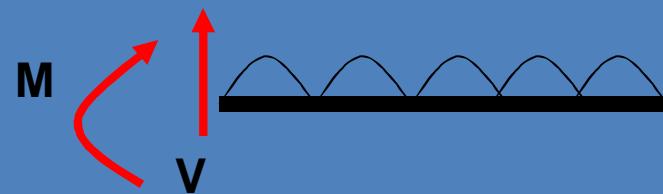
Real Moment, M



LHS

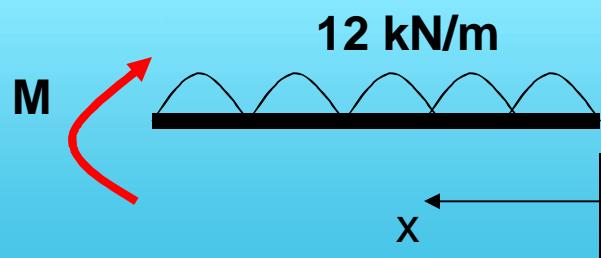


RHS



Real Moment, M

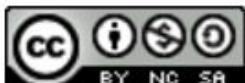
RHS



$$\sum M_x = 0 \text{ (clockwise +ve)}$$

$$M + \frac{12x^2}{2} = 0$$

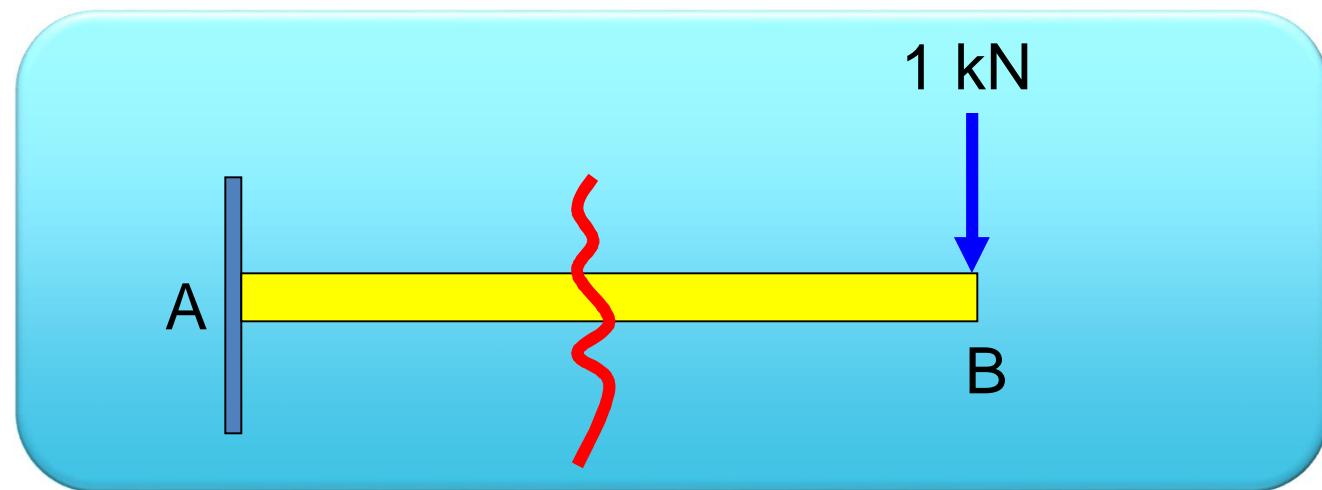
$$M = -6x^2$$



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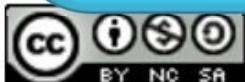
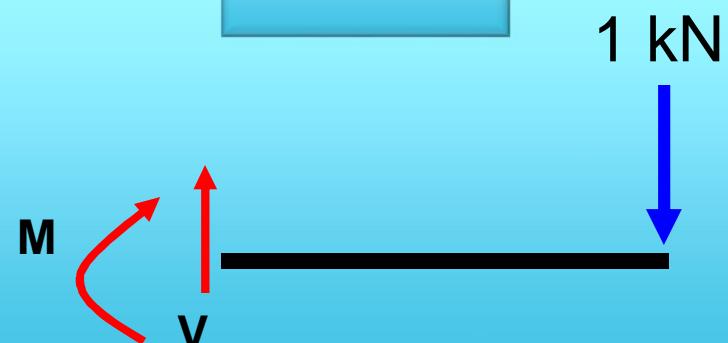
Virtual Moment, m



LHS



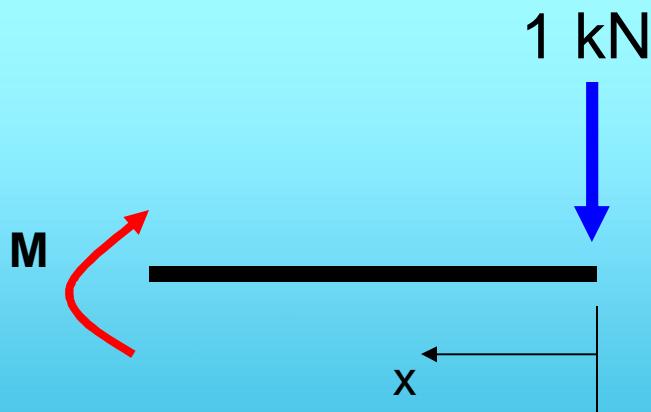
RHS



Virtual Moment, m

Considered RHS

$0 < x < 10$



$$\sum M_x = 0 \text{ (clockwise +ve)}$$

$$m + 1 \cdot x = 0$$

$$m = -1 \cdot x$$



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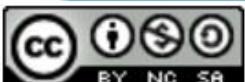
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Virtual-Work Equation

$$\begin{aligned}
 1kN.\Delta &= \int_0^L \frac{mM}{EI} dx \\
 &= \int_0^{10} \frac{(-x)(-6x^2)}{EI} dx \\
 &= \frac{15 \times 10^3 kN.m^3}{EI}
 \end{aligned}$$

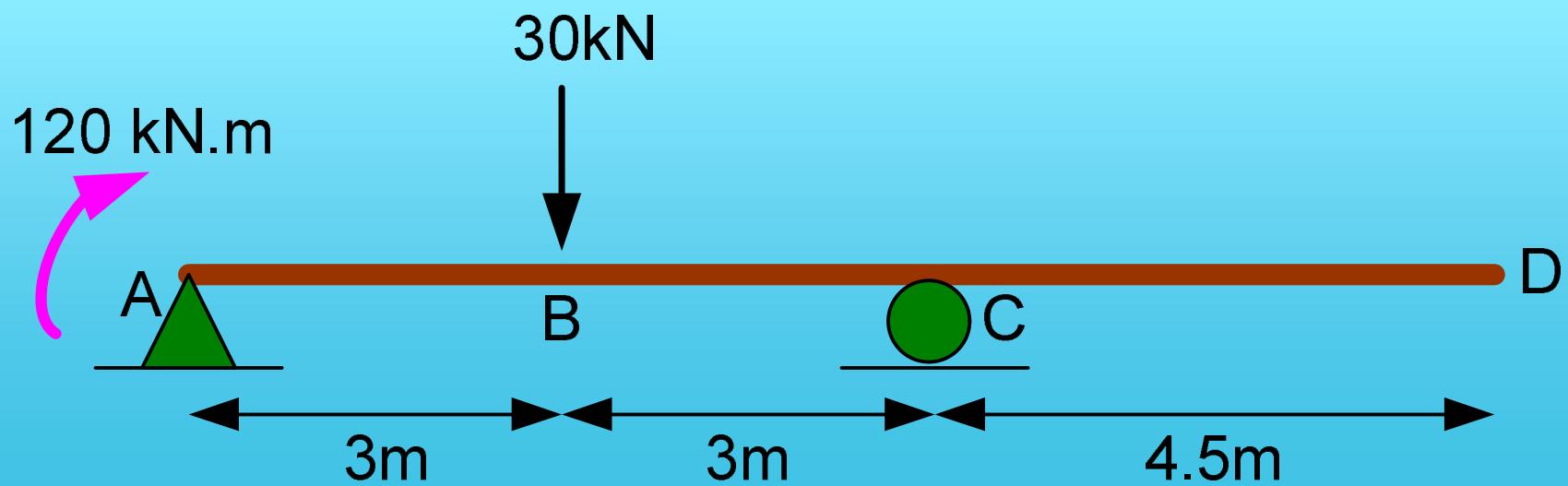
OR

$$\begin{aligned}
 \Delta_B &= \frac{15 \times 10^3 kN.m^3}{200(10^6)kN/m^2(500(10^6)mm^4)(10^{-12}m^4/mm^4)} \\
 &= 0.150m \quad = 150mm
 \end{aligned}$$



Example 2

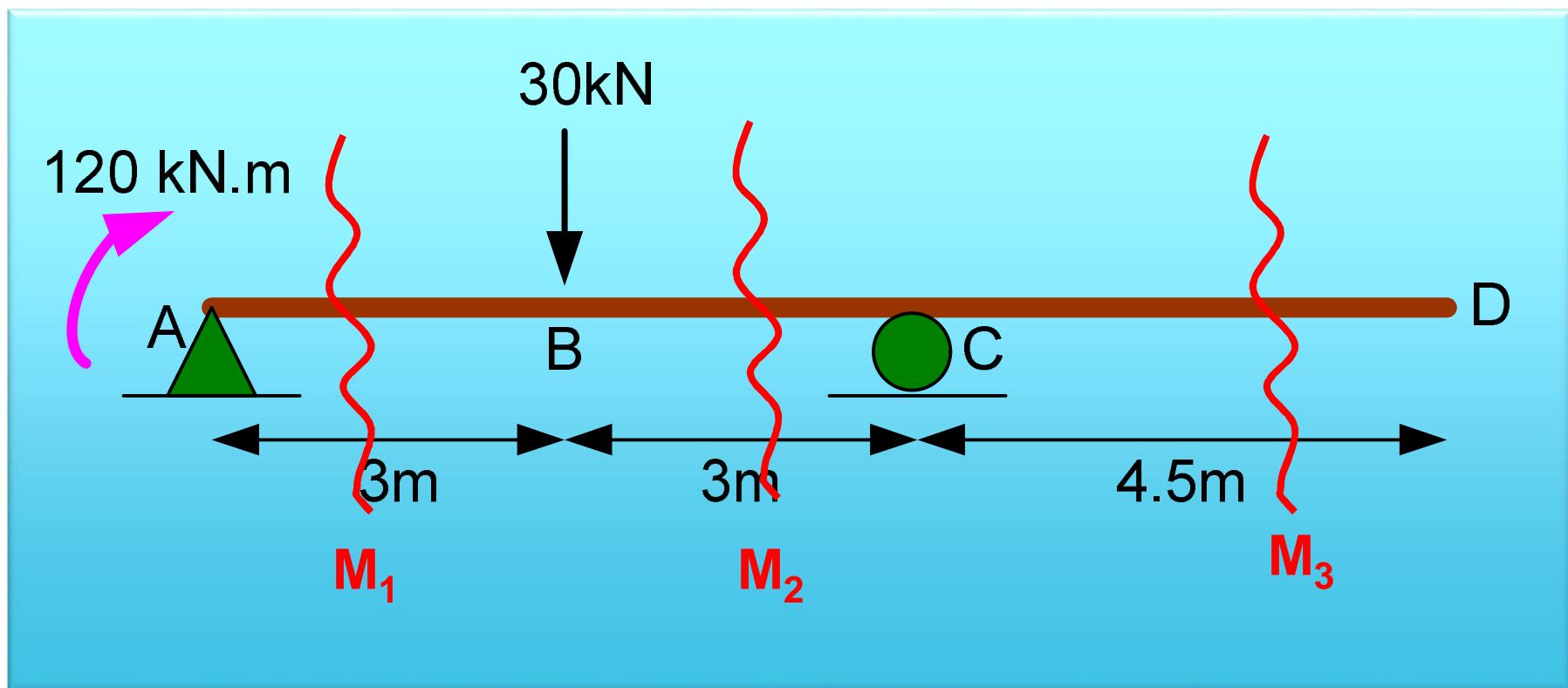
Determine the displacement at D of the steel beam in figure. Take $E = 200\text{GPa}$, $I = 300\text{E}6 \text{ mm}^4$



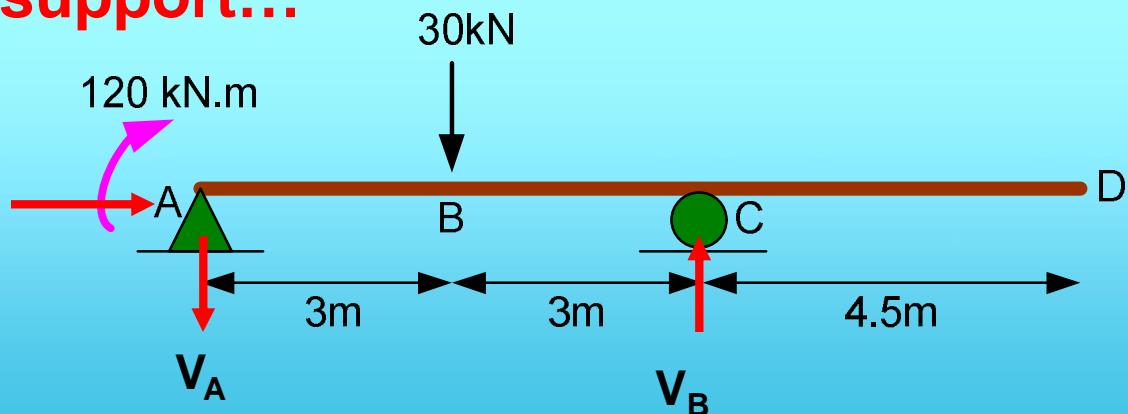
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Real Moment, M



Determine the reaction at support...



$$\sum M_A = 0 \text{ (clockwise + ve)}$$

$$120 + 30(3) - V_B(6) = 0$$

$$V_B = 35\text{kN}$$

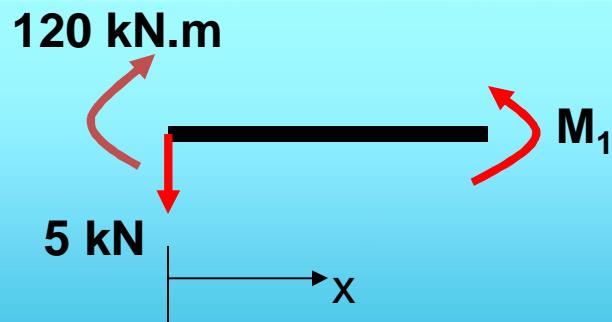
$$\sum F_y = 0 \text{ (upward + ve)}$$

$$-V_A + 35 - 30 = 0$$

$$V_A = 5\text{kN}$$

Member AB : LHS

$$0 \leq x \leq 3$$



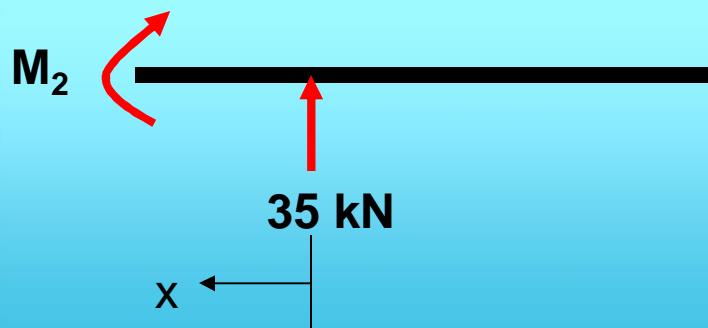
$$\sum M_x = 0 \text{ (clockwise + ve)}$$

$$-M_1 - 5(x) + 120 = 0$$

$$M_1 = 120 - 5x$$

Member BC : RHS

$$0 \leq x \leq 3$$



$$\sum M_x = 0 \text{ (clockwise + ve)}$$

$$M_2 - 35(x) = 0$$

$$M_2 = 35(x)$$

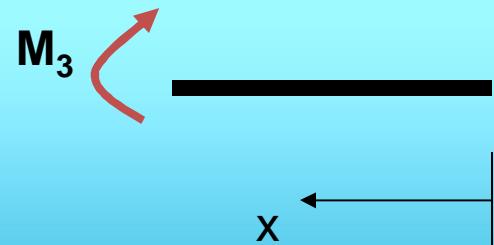


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Member CD : RHS

$$0 \leq x \leq 4.5$$



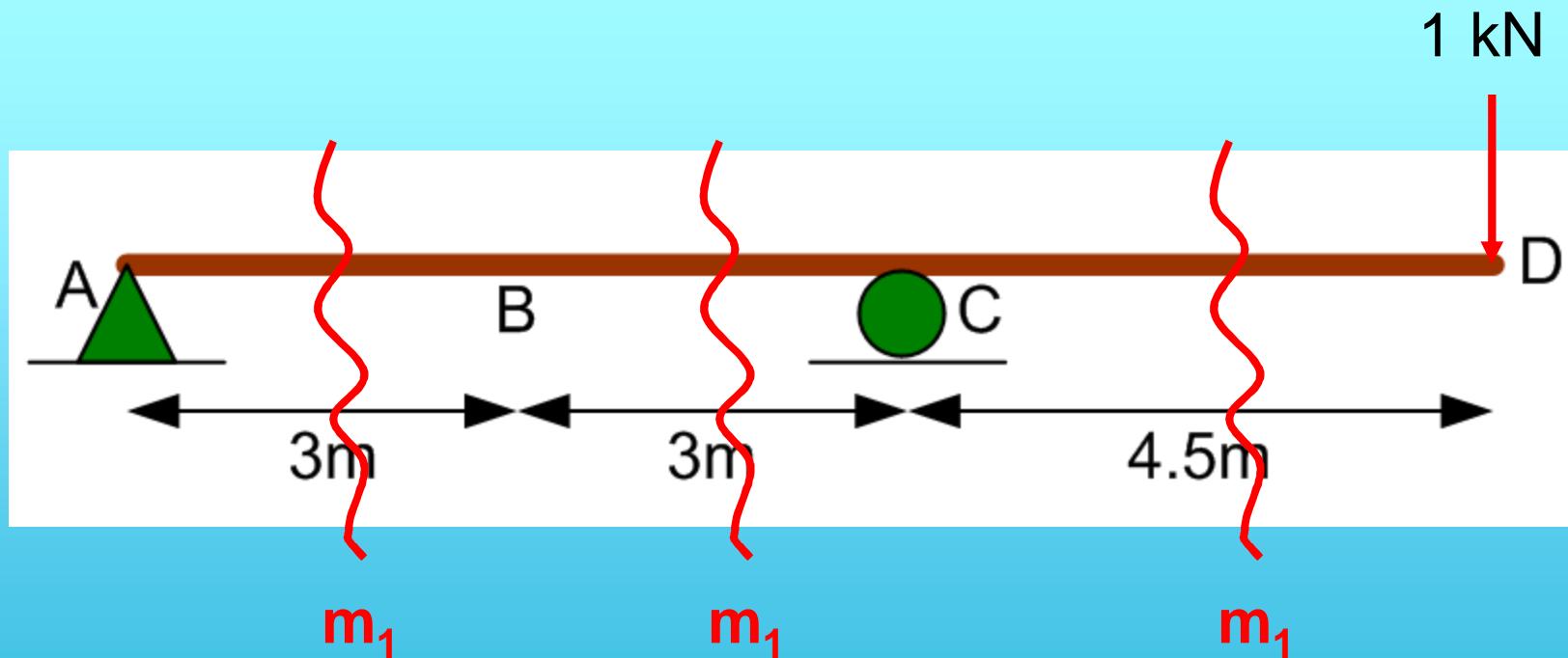
$$\sum M_x = 0 \text{ (clockwise + ve)}$$
$$M_3 = 0$$



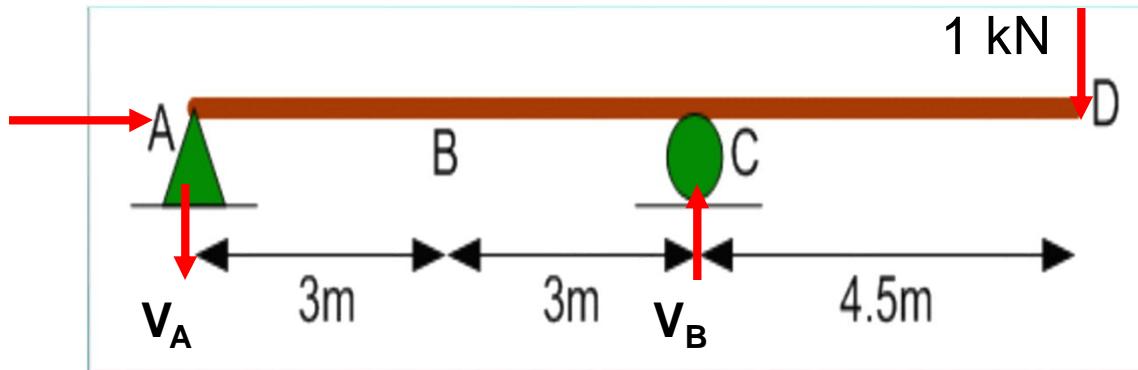
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Virtual moment, m



Determine the reaction at support



$$\sum M_A = 0 \text{ (clockwise + ve)}$$

$$1(10.5) - V_B(6) = 0$$

$$V_B = 1.75kN$$

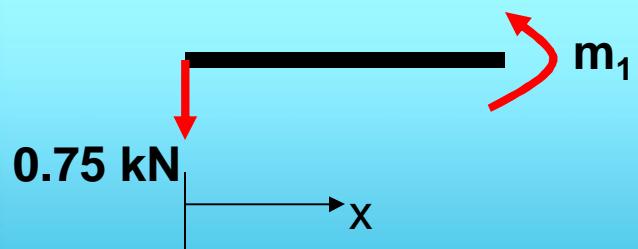
$$\sum F_y = 0 \text{ (upward + ve)}$$

$$-V_A + 1.75 - 1 = 0$$

$$V_A = 0.75kN$$

Member AB : LHS

$$0 \leq x \leq 3$$



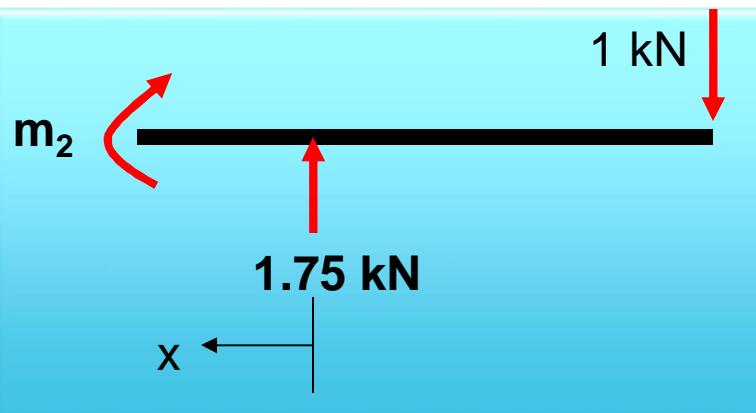
$$\sum M_x = 0 \text{ (clockwise +ve)}$$

$$-m_1 - 0.75(x) = 0$$

$$m_1 = -0.75x$$

Member BC : RHS

$$0 \leq x \leq 3$$



$$\sum M_x = 0 \text{ (clockwise +ve)}$$

$$m_2 - 1.75(x) + 1(x + 4.5) = 0$$

$$m_2 = 0.75(x) - 4.5$$

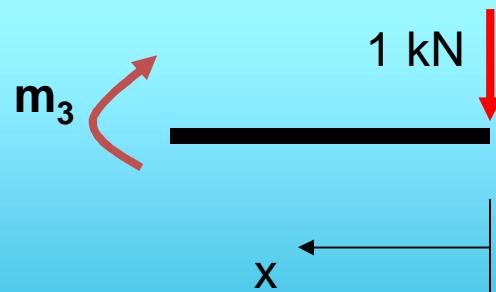


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Member CD : RHS

$$0 \leq x \leq 4.5$$



$$\sum M_x = 0 \text{ (clockwise +ve)}$$

$$m_3 + 1 \cdot x = 0$$

$$m_3 = -x$$



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Virtual-Work Equation

$$\begin{aligned}
 1kN.\Delta_d &= \int_0^L \frac{mM}{EI} dx \\
 &= \int_0^3 \frac{m_1 M_1}{EI} dx + \int_0^3 \frac{m_2 M_2}{EI} dx + \int_0^{4.5} \frac{m_3 M_3}{EI} dx \\
 &= \int_0^3 \frac{(-0.75x)(120 - 5x)}{EI} dx + \int_0^3 \frac{(0.75x - 4.5)(35x)}{EI} dx \\
 &\quad + \int_0^{4.5} \frac{(-x)(0)}{EI} dx
 \end{aligned}$$



$$\Delta_D = -\frac{371.25}{EI} - \frac{472.5}{EI} + \frac{0}{EI}$$

$$= -\frac{843.75 \text{ kN} \cdot \text{m}^3}{EI}$$

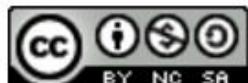
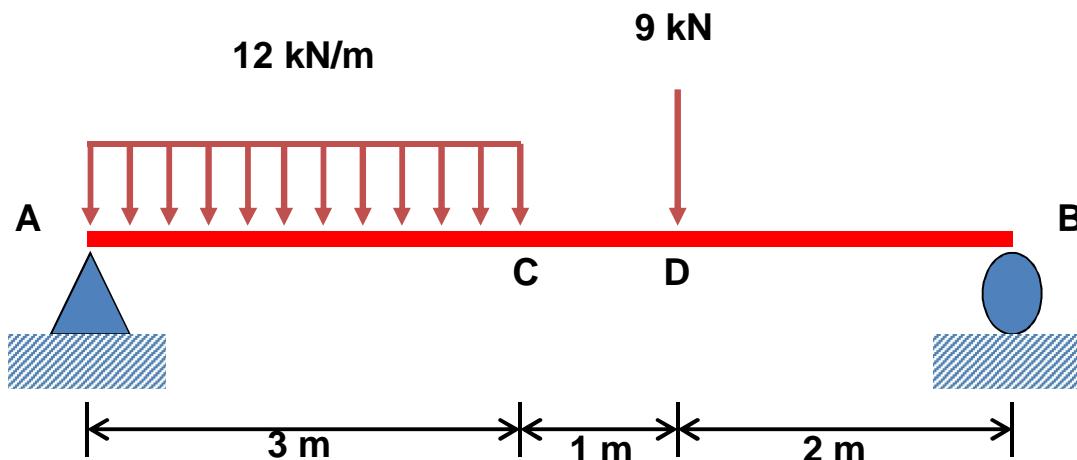
$$\Delta_D = \frac{-843.75 \text{ kN} \cdot \text{m}^3}{200(10^6) \text{ kN} / \text{m}^2 (300(10^6) \text{ mm}^4)(10^{-12} \text{ m}^4 / \text{mm}^4)}$$

$$= -0.0141 \text{ m} \quad = -14.1 \text{ mm}$$



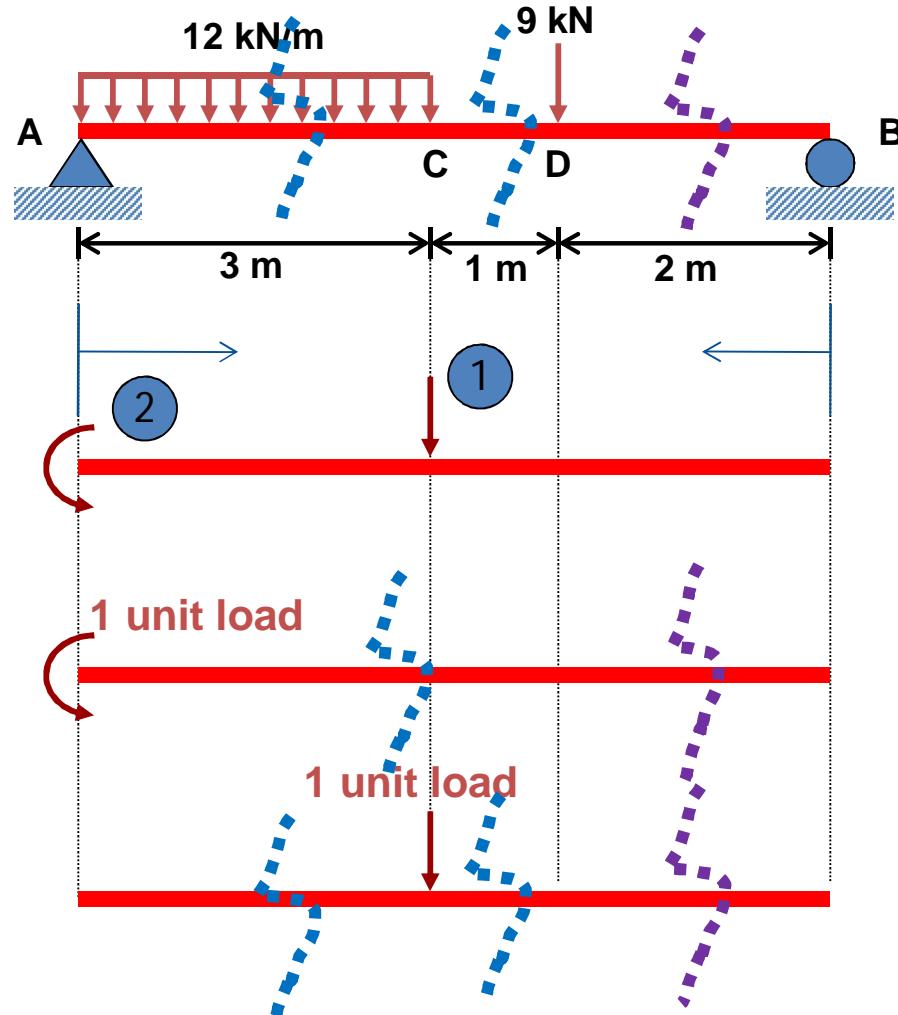
Example 3

Determine the **slope** at A and **deflection** at C in the beam shown below



Solution

Real Load (M)



Generalized coordinates

Virtual Load (m_θ): Slope

Virtual Load (m_Δ): Deflection

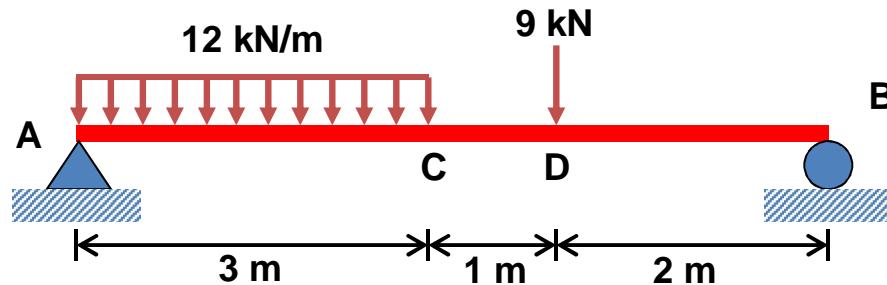


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Real Load → M ?

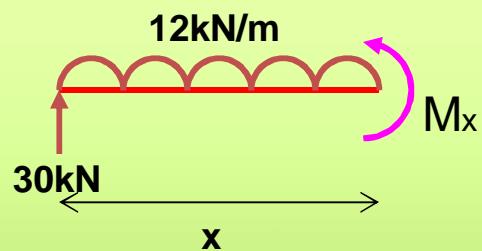
1. Support reaction,



$$\begin{aligned}\sum M_A &= 0 \text{ (clockwise +),} \\ -R_B(6) + 9(4) + 12(3)\left(\frac{3}{2}\right) &= 0 \\ \therefore R_B &= 15kN\end{aligned}$$

$$\begin{aligned}\sum F_y \uparrow^+ &= 0, \\ R_A - 12(3) - 9 + 15 &= 0 \\ \therefore R_A &= 30kN\end{aligned}$$





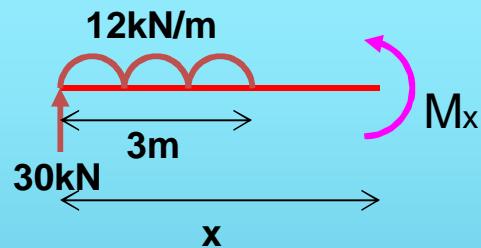
Real Load (M) : $0 \leq x \leq 3$ (*segment AC*)

$$\sum M_x = 0 \text{ (clockwise+)},$$

$$M_x = 30x - 12\left(\frac{x^2}{2}\right)$$

$$\therefore M_x = 30x - 6x^2 \dots\dots\dots(i)$$





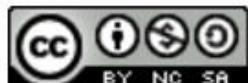
Real Load (M): $3 \leq x \leq 4$ (*segment CD*)

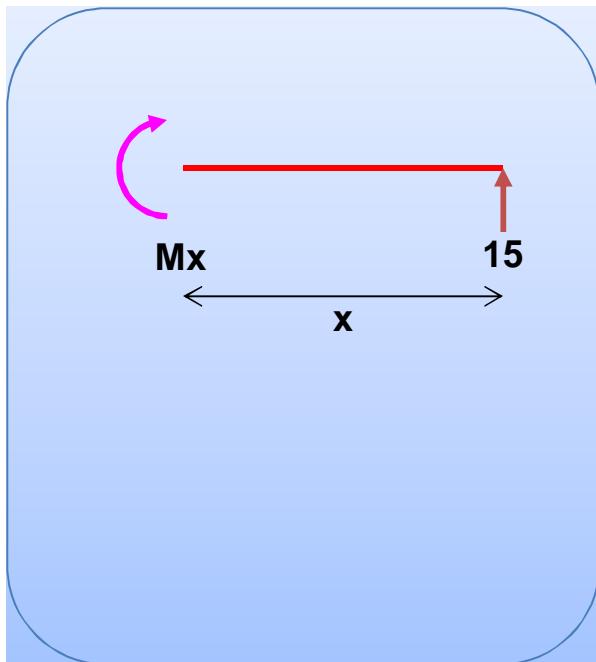
$$\sum M_x = 0 \text{ (clockwise +),}$$

$$M_x = 30x - 12(3)(x - \frac{3}{2})$$

$$M_x = 30x - 36x + 54$$

$$\therefore M_x = -6x + 54 \dots\dots\dots (ii)$$





Real Load (M) : $0 \leq x \leq 2$ (*segment BD*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

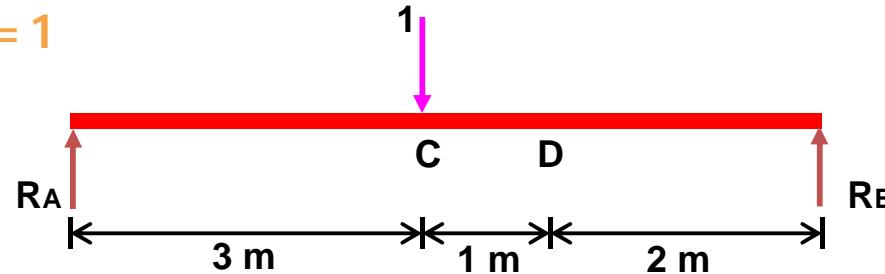
$$-M_x = -15x$$

$$\therefore M_x = 15x \dots\dots\dots(iii)$$



Virtual Load, m for deflection

Apply point load $P= 1$

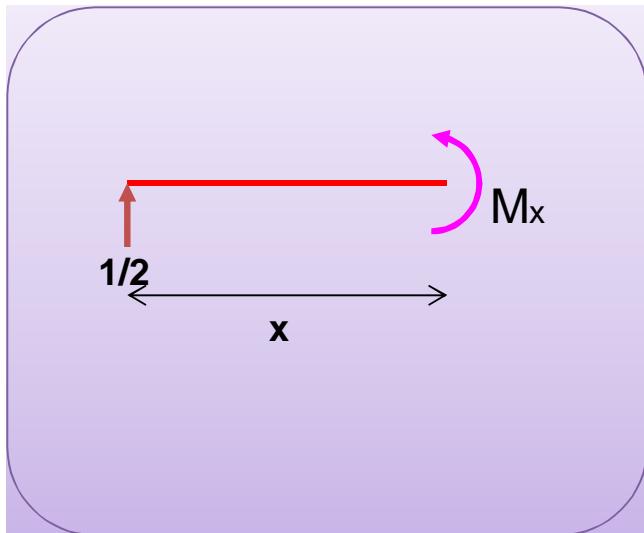


$$\begin{aligned}\sum M_A &= 0 \text{ (clockwise +),} \\ -R_B(6) + 1(3) &= 0\end{aligned}$$

$$\therefore R_B = \frac{1}{2}$$

$$\begin{aligned}\sum F_y \uparrow^+ &= 0, \\ R_A + R_B - 1 &= 0 \\ \therefore R_A &= \frac{1}{2}\end{aligned}$$



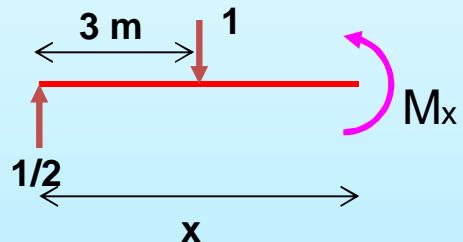


Virtual Load (m) : $0 \leq x \leq 3$ (*segment AC*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

$$\therefore M_x = \frac{1}{2}x \dots\dots\dots(i)$$





Virtual Load (m) : $3 \leq x \leq 4$ (*segment CD*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

$$\therefore M_x = -0.5x + 3 \dots\dots\dots(ii)$$



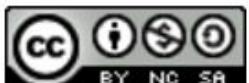


Virtual Load (m) : $0 \leq x \leq 2$ (*segment BD*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

$$-M_x = -\frac{1}{2}x$$

$$\therefore M_x = \frac{1}{2}x \dots\dots\dots(iii)$$



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Deflection at C, Δ_D :

$$\Delta_D = \int \frac{Mm}{EI} dx$$

$$= \frac{1}{EI} \int_0^3 (30x - 6x^2)(0.5x)dx + \frac{1}{EI} \int_3^4 (-6x + 54)(-0.5x + 3)dx$$

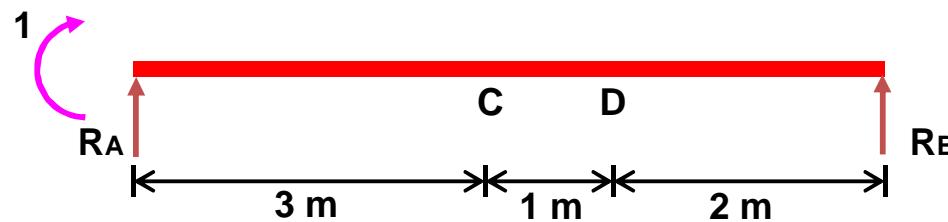
$$\frac{1}{EI} \int_0^2 (15x)(0.5x)dx$$

$$= \frac{135.75}{EI}$$



Virtual Load, m for rotation

Apply $m_\theta = 1$



$$\sum M_A = 0 \text{ (clockwise +),}$$

$$-R_B(6) + 1 = 0$$

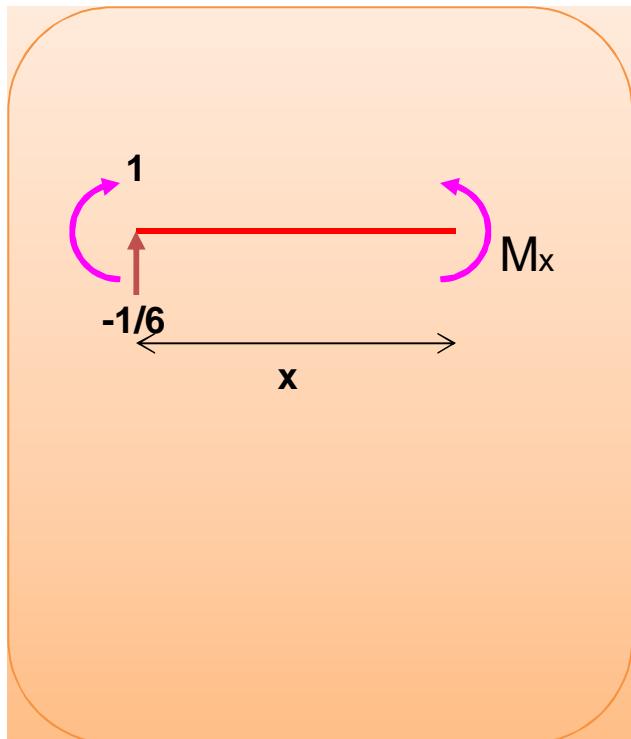
$$\therefore R_B = \frac{1}{6}$$

$$\sum F_y \uparrow^+ = 0,$$

$$R_A + R_B = 0$$

$$\therefore R_A = -\frac{1}{6}$$





Virtual Load (m) : $0 \leq x \leq 3$ (*segment AC*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

$$\therefore M_x = 1 - \frac{1}{6}x \dots\dots\dots(i)$$



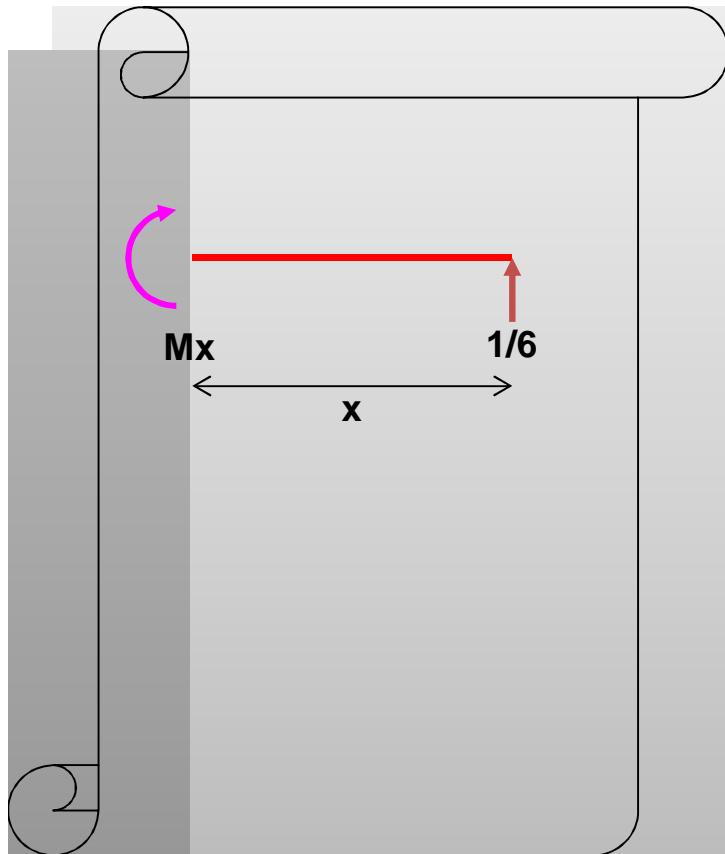


Virtual Load (m) : $3 \leq x \leq 4$ (*segment CD*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

$$\therefore M_x = 1 - \frac{1}{6}x \dots\dots\dots(ii)$$





Virtual Load (m) : $0 \leq x \leq 2$ (*segment BD*)

$$\sum M_x = 0 \text{ (clockwise +),}$$

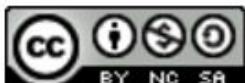
$$-M_x = -\frac{1}{6}x$$

$$\therefore M_x = \frac{1}{6}x \dots\dots\dots(iii)$$



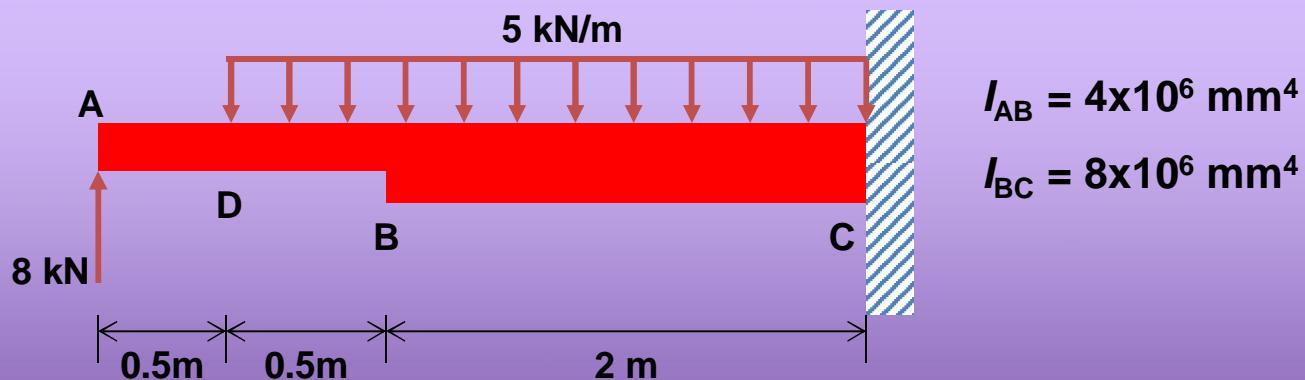
Slope at A, θ_A :

$$\begin{aligned}\theta_A &= \int \frac{Mm}{EI} dx \\ &= \frac{1}{EI} \int_0^3 (30x - 6x^2) \left(1 - \frac{x}{6}\right) dx + \frac{1}{EI} \int_3^4 (-6x + 54) \left(1 - \frac{x}{6}\right) dx \\ &\quad - \frac{1}{EI} \int_0^2 (15x) \left(\frac{x}{6}\right) dx \\ &= \frac{76.75}{EI}\end{aligned}$$



Example 4

Determine the **slope and deflection at B** in the beam shown below. Given
 $E=200 \text{ kN/mm}^2$



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Moment equation (deflection):

Segment	Condition	$I \text{ mm}^4$	$m \text{ (deflection)}$	M
AD	$0 < x < 0.5$	4×10^6	0	$8x$
DB	$0.5 < x < 1$	4×10^6	0	$8x - 2.5(x - 0.5)^2$
BC	$1 < x < 3$	8×10^6	$x - 1$	$8x - 2.5(x - 0.5)^2$



Deflection, Δ_B

$$\Delta_B = \int \frac{mM}{EI} dx$$

$$= \int_1^3 \frac{(x-1)(-2.5x^2 + 10.5x - 0.625)}{(200 \times 10^6)(8 \times 10^{-6})} dx$$

$$= \frac{1}{1600} \left[-\frac{2.5x^4}{4} + \frac{13x^3}{3} - \frac{11.125x^2}{2} + 0.625x \right]_1^3$$

$$= 0.012m$$

$$= 12mm$$



Moment equation (slope):

Segment	Condition	$I \text{ mm}^4$	m (slope)	M
AD	$0 < x < 0.5$	4×10^6	0	$8x$
DB	$0.5 < x < 1$	4×10^6	0	$8x - 2.5(x - 0.5)^2$
BC	$1 < x < 3$	8×10^6	-1	$8x - 2.5(x - 0.5)^2$



Slope, θ_B

$$\begin{aligned}
 \theta_B &= \int \frac{mM}{EI} dx \\
 &= \int_1^3 \frac{(1)(-2.5x^2 + 10.5x - 0.625)}{(200 \times 10^6)(8 \times 10^{-6})} dx \\
 &= \frac{1}{1600} \left[-\frac{2.5x^3}{3} + \frac{10.5x^2}{2} - 0.625x \right]_1^3 \\
 &= \frac{19.1}{1600} \\
 &= 0.0119 \text{ rad}
 \end{aligned}$$



THANKS



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